

1 **Compact mid-infrared dual-comb spectrometer over 3-4 μm**
2 **via intrapulse difference frequency generation in LiNbO_3**
3 **waveguide**

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15 **Abstract:** Mid-infrared optical frequency comb is a powerful tool for gas sensing. In this study,
16 we demonstrate a simple mid-infrared dual-comb spectrometer covering 3–4 μm in LiNbO_3
17 waveguide. Based on a low-power fiber laser system, the mid-infrared comb is achieved via intra-
18 pulse difference frequency generation in the LiNbO_3 waveguide. We construct pre-chirp
19 management before supercontinuum generation to control spatiotemporal alignment for pump and
20 signal pulses. The supercontinuum is directly coupled into a chirped periodically poled LiNbO_3
21 waveguide for the 3–4 μm idler generation. A mid-infrared dual-comb spectrometer based on this
22 approach provides a 100 MHz resolution over 25 THz coverage. To evaluate the applicability for
23 spectroscopy, we measure the methane spectrum using the dual-comb spectrometer. The measured
24 results are consistent with HITRAN database, which the root mean square of the residual is 3.2%.

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25 This proposed method is expected to develop integrated and robust mid-infrared dual-comb
26 spectrometers on chip for sensing.

27 *Key words: nonlinear optics; dual-comb spectroscopy; difference frequency generation; mid-*
28 *infrared gas sensing*

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30

I. Introduction

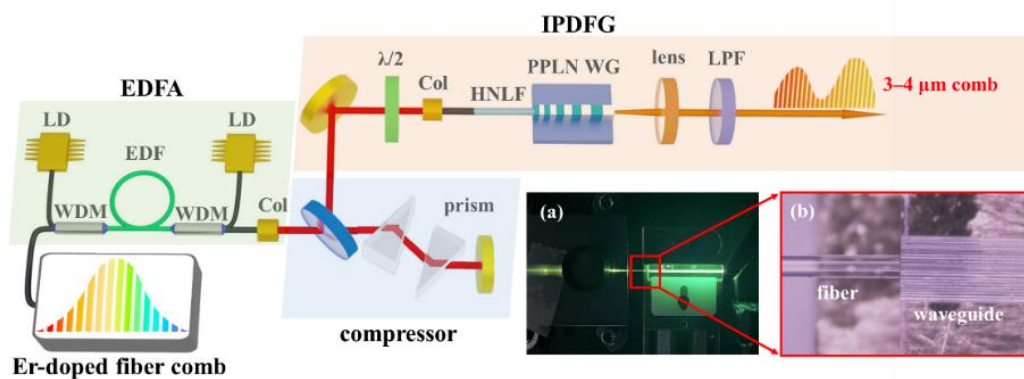
31 Optical frequency combs are powerful tools for rapid gas sensing. In particular, frequency comb
32 spectroscopy in the mid-infrared (MIR, 3–5 μm) region of the atmospheric window has made
33 significant progress in various applications, such as greenhouse gas monitoring, atmospheric
34 monitoring, green agriculture, and breath analysis [1–4]. Generally, these MIR frequency combs
35 can be obtained via $\chi^{(2)}$ and $\chi^{(3)}$ nonlinear processes in lithium niobate (LN) [5–9], which is a
36 widely used optical material that can provide wide transparency window, high nonlinear
37 coefficient, and electro-optical effect for integrated chip-based laser devices [10]. In comparison
38 with bulk crystals, periodically poled LN (PPLN) waveguides with strong light confinement ensure
39 high-efficiency nonlinear frequency conversion over a long interaction path. Therefore, PPLN
40 waveguides allow low-power near-infrared (NIR) laser systems to perform efficient nonlinear
41 processes and scale their spectra to the MIR region [11–14]. MIR sources based on LN waveguides
42 have small size and low power consumption, making them ideal for the construction of integrated
43 MIR frequency comb equipment. In addition, the dual-comb spectroscopy (DCS) system can
44 realize high-resolution rapid spectral measurements by employing a single photodetector [15, 16].
45 DCS combined with the photonic technology can significantly reduce the equipment size and
46 facilitate the development of portable gas sensors. Numerous integrated frequency combs based
47 on microresonators, interband cascade lasers or diode lasers have been demonstrated for
48 spectroscopy [17–19].

49 MIR spectroscopy offers high sensitivity for molecular sensing. However, limited spectral
50 bandwidth and complex phase control pose two major challenges in demonstrating the
51 technological advantages of DCS in the MIR region. To meet the bandwidth requirements,
52 nonlinear conversion methods have been developed to broaden the spectra to the MIR region,
53 including supercontinuum generation (SCG), difference frequency generation (DFG), and optical
54 parametric oscillators (OPO) [20]. State-of-the-art broadband MIR dual-comb systems have been
55 achieved via DFG and OPO, which have also been successfully applied in comb-line resolved
56 DCS and multispecies detection of trace gases [21–24]. Generally, the DFG system, which can
57 passively stabilize the carrier-envelope phase of the MIR comb, consists of the noncollinear pump
58 and signal branches from the same seed laser. In this two-branch structure, delay control is required
59 to stabilize the pump-signal pulses walk-off in the time domain and suppress the intensity noise of
60 MIR pulses [25]. Recently, several studies have reported the simple method of MIR comb
61 generation via intra-pulse DFG (IPDFG) [26–30]. Through precise chirp management of the
62 supercontinuum, a single branch can provide natural spatiotemporal alignment for the pump and
63 signal pulses, achieving multi-octave-spanning MIR combs [26–28]. The potential of these simple

64 IPDFG MIR systems for high-resolution DCS has been demonstrated in the past [29, 30]. By
 65 combining the IPDFG and PPLN waveguides, a broadband MIR comb source was realized with
 66 an integrated and simple structure [31]. Therefore, we believe that a portable gas-sensing
 67 instrument can be developed using DCS and IPDFG combs on a LN waveguide.

68 In this study, a simple 3–4 μm MIR dual-comb spectrometer with waveguide-based IPDFG
 69 modules is demonstrated. We constructed an Er-doped fiber dual-comb system as the seed source.
 70 To realize the spatiotemporal alignment of the pump and signal pulses, the front prism pair
 71 provides easily adjustable pre-chirp control for the soliton self-compression in a highly nonlinear
 72 fiber (HNLf). The broadband MIR combs over the 3–4 μm region were yielded from high-
 73 efficiency chirped PPLN waveguides via the IPDFG process. Thereafter, the comb-line-resolved
 74 DCS with 100 MHz spectral resolution over 25 THz coverage was demonstrated. Finally, we
 75 measured the absorption spectrum of methane to verify the applicability of the MIR dual-comb
 76 system for precision spectroscopy. We compared the measured result with the HITRAN database,
 77 and the root mean square (RMS) of the residual is 3.2%. This dual-comb system without phase
 78 correction enables mode-resolved DCS with a figure of merit of 1.03×10^6 . Thus far, femtosecond
 79 lasers, frequency combs, amplifiers, and SCG on chips have been successfully demonstrated [32–
 80 34]. The MIR comb generation method, which does not require the detection of offset frequency
 81 of MIR pulses, is conducive to low-power sources on chips. We believe that this approach
 82 contributes to the development of broadband MIR frequency combs and portable DCS systems on
 83 chips.

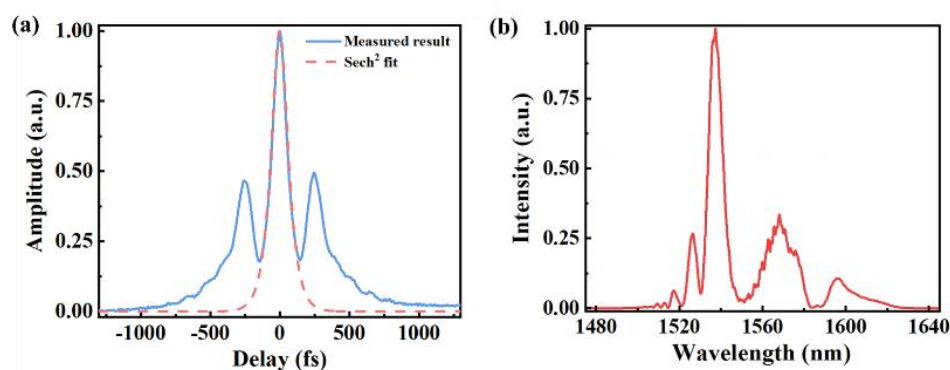
84 II. Experimental setup and results



85
 86 Fig. 1. Schematic of the MIR comb generation. The lens after the waveguide to make the
 87 schematic look easier to understand. In the actual system, we use an off-axis parabolic mirror
 88 to collimate the MIR light instead of the lens. LD: laser diode; EDF, Er-doped fiber; WDM,
 89 wavelength division multiplexer; Col: collimator; EDF, Er-doped fiber amplifier; $\lambda/2$, half-

90 wave plate; HNLf, highly nonlinear fiber; PPLN WG, periodically poled lithium niobate
 91 waveguide; and LPF, long-pass filter. Moreover, we also recorded the images of the PPLN WG
 92 using a phone camera (insert a) and a CCD camera (insert b).

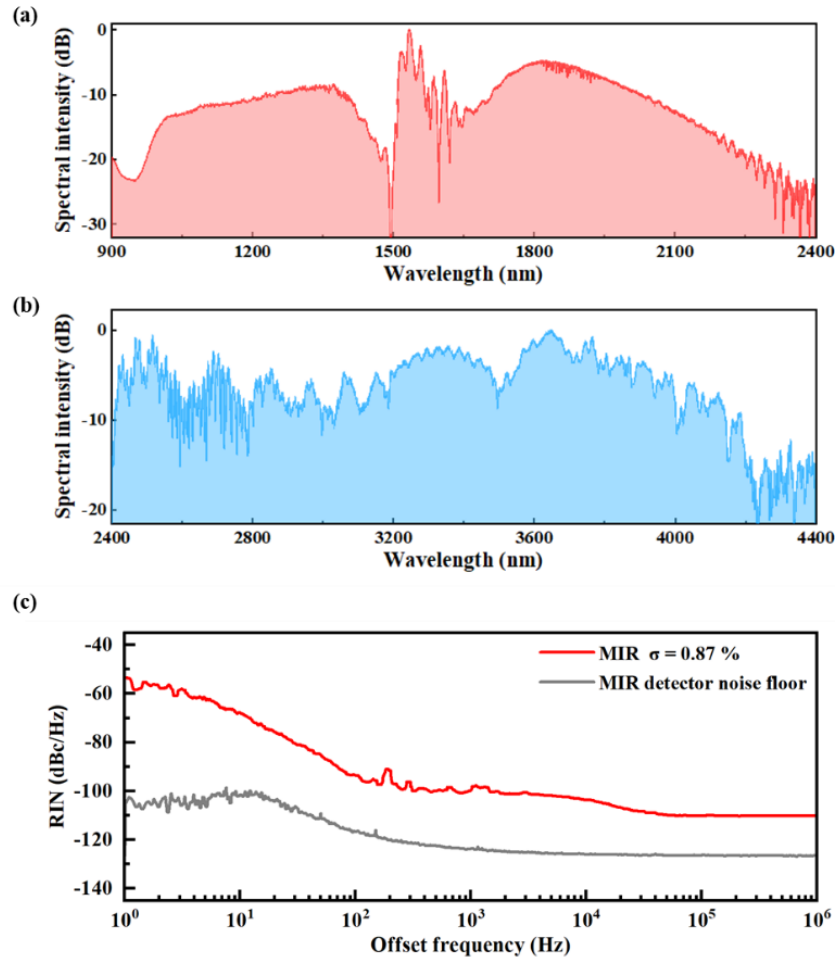
93 The schematic of the MIR comb generation is shown in Figure 1, which includes a seed comb
 94 centered at 1.5 μm , Er-doped fiber amplifier, prism compressor, HNLf, and IPDFG module. The
 95 seed comb based on an Er-doped fiber mode-locked laser emitted a pulse train with a 1 mW
 96 average power and a 100 MHz repetition rate. The average pulse power was scaled up to 328 mW
 97 using a bidirectionally pumped fiber amplifier, in which a 3 m Er-doped single-mode fiber with a
 98 normal dispersion was used as the gain medium. A pair of silicon prisms was adopted to provide
 99 controllable anomalous dispersion for pre-chirp management of SCG. Linearly polarized light was
 100 injected into the dispersion prisms at a Brewster angle to reduce the reflection loss on the prism
 101 surfaces. Behind the prism compression, 300 mW laser was coupled to a collimator with 12 cm
 102 PM1550 pigtail fiber, which could further recompress the pulse duration. Figure 2(a) and (b) are
 103 the autocorrelation curve and spectrum after the prism compressor respectively. The pulse duration
 104 is 92 fs with sech^2 fitting, and the spectrum covers the range from 1520 nm to 1620 nm. The large
 105 pulse wings are caused by uncompensated nonlinear chirp. 3 cm PM HNLf with an anomalous
 106 dispersion of 1.9 ps/(nm·km) was employed to generate a supercontinuum spectrum. The spectral
 107 broadening and soliton self-compression processes in the anomalous-dispersion HNLf were
 108 adjusted using the prism-based pre-chirp management module.



109
 110 Fig. 2. (a) Autocorrelation trace and (b) Measured spectrum of the compressor output.

111 To drive the IPDFG and yield MIR light, the supercontinuum from the HNLf was directly
 112 coupled to a chirped PPLN waveguide. The HNLf is placed on a 3-axis stage to launch light to
 113 the waveguide. A zoom lens and camera system on the top of the waveguide were used for high-
 114 magnification imaging. By adjusting the stage, we can get the optimal alignment and measure the
 115 output light. The mode diameter of HNLf is 3.5 μm . This PPLN waveguide is 15 μm wide and 25
 116 mm long with aperiodic periods of 23–32 μm that were consistent with our previous study [35].
 117 The coupling efficiency is 60%. In general, some spatial optical components, including wedge and
 118 chirp mirrors, were required to control the pulse chirp before IPDFG [26, 28]. These extra spatially
 119 manipulated modules increased total loss and system complexity. In particular, we did not adopt
 120 common methods for controlling the chirp but simply adjusted the prism pair before the
 121 anomalous-dispersion HNLf to optimize the temporal alignment of pump-signal pulses with the

122 soliton self-compression effect [27, 36–38]. In addition, these prisms could be removed completely
 123 to simplify the system for integrated MIR comb generation [31]. Thereafter, a gold-coated off-axis
 124 parabolic mirror with a focal distance of 6 mm collimated the light to free space. Finally, a long-
 125 pass filter at 2.4 μm was used to filter out the residual pump and signal light, outputting MIR
 126 frequency comb with a high transmissivity.

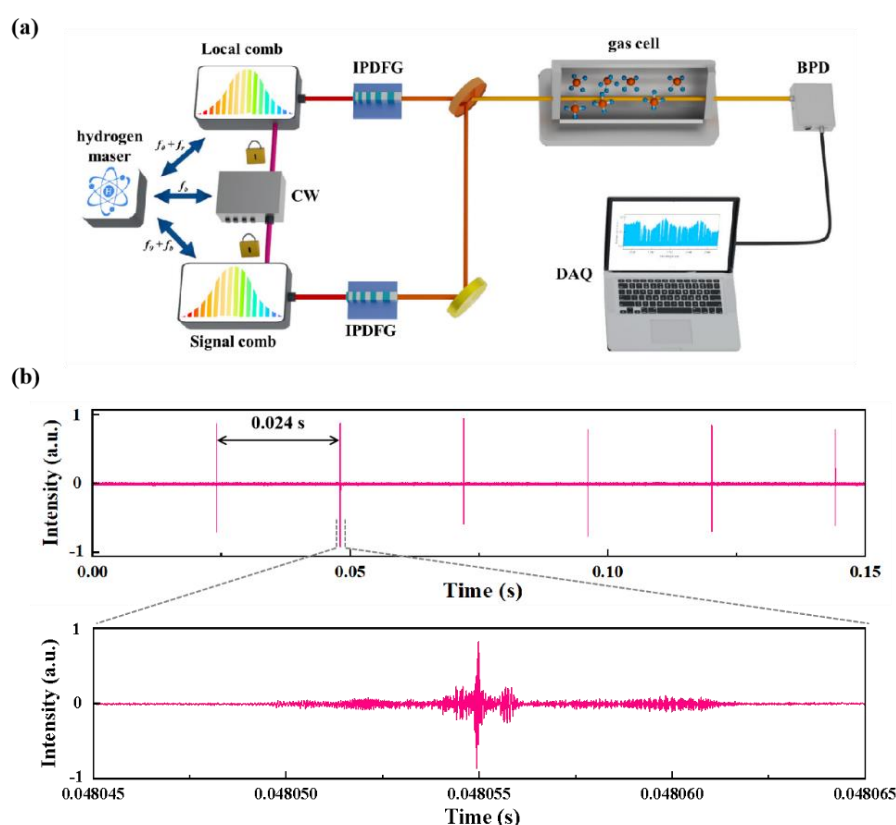


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128 Fig. 3. (a) Spectral profile of SCG. The spectral region is separately measured using Yokogawa
 129 AQ6370 (900–1700 nm) and Bristol 771B (1700–2400 nm). (b) The spectral profile of the MIR
 130 comb. (c) The RIN of MIR light.

131 To characterize the spectral evolution of the SCG and IPDFG, we measured the corresponding
 132 spectral profiles using two commercial spectrometers (Yokogawa AQ6370 and Bristol 771B). The
 133 HNLFF delivers 150 mW supercontinuum with a spectral range of 1–2 μm , as shown in Fig. 3(a).
 134 Theoretically, this supercontinuum spectrum can provide the pump and signal light for 2–5 μm
 135 idler generation. In addition, absorption lines were observed at approximately 1900 nm owing to
 136 water vapor in the air. To maximize the conversion efficiency of the IPDFG, the slow axis of the
 137 HNLFF was rotated to ensure that the pump and signal lights were coupled to the waveguide with
 138 vertical polarization. After the filter, 0.7 mW MIR light was obtained. The spectrum was measured

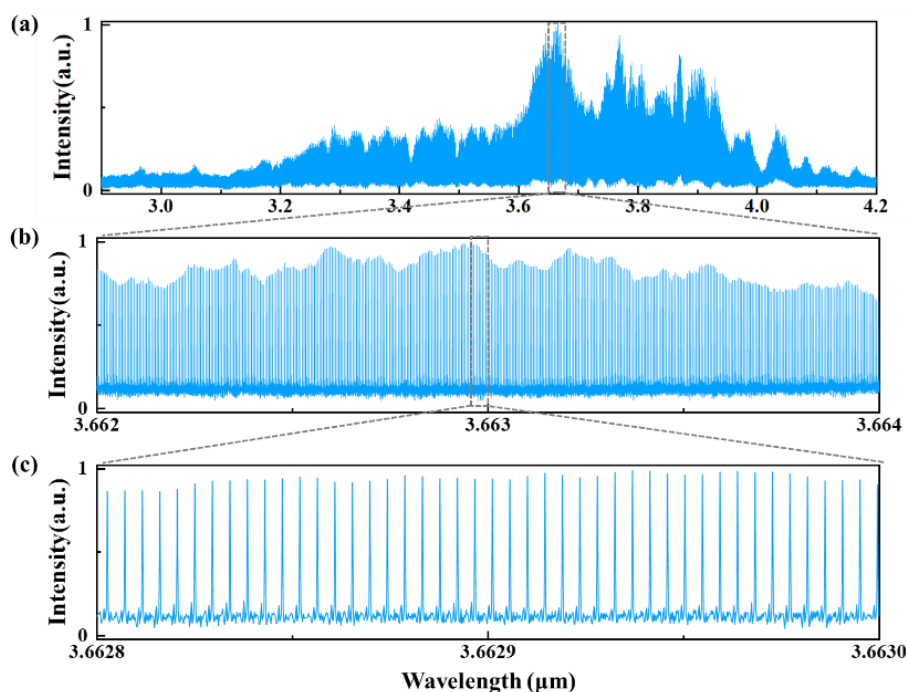
139 using a Fourier-transform spectrometer (Bristol 771 B) with a 33 GHz spectral resolution, as
 140 shown in Fig. 3(b). We observed that the long wavelength was cut off at 4.2 μm , which was not as
 141 broad as expected. The most likely reason is that the waveguide channel brought different group
 142 velocity dispersions to the pump and signal pulses, which caused temporal misalignment of the
 143 pump and signal pulses. In addition, the effect of waveguide dispersion on the refractive index is
 144 ignored, so the poling periods are not optimal. In future studies, dispersion engineering and poling
 145 periods should be considered to redesign the waveguide and broaden the MIR spectrum [39]. We
 146 measured the relative intensity noise (RIN) of MIR light, as shown in Fig. 3(c). The integrated
 147 RIN is 0.87%.



148
 149 Fig. 4. (a) Schematic of the MIR dual-comb system. The recorded interferograms at different
 150 time scales of (b) 150 and (c) 0.02 ms. CW: continuous laser; BPD, balanced photodetector;
 151 DAQ, data acquisition.

152 A dual-comb spectrometer based on the IPDFG method was constructed for DCS measurement,
 153 as shown in Fig. 4(a). Two Er-doped fiber comb systems served as the seed combs. The NIR local
 154 comb ($f_{0_comb1} = 20$ MHz and $f_{r_comb1} = 100$ MHz) was referenced to the hydrogen maser clock. A
 155 10 Hz linewidth CW laser centered at 1560 nm (OE4030, OEwaves) was referenced to the local
 156 comb to provide a standard optical frequency reference for the signal comb. To stabilize the signal
 157 comb, the carrier-envelope-phase offset frequency ($f_{0_comb2} = 20$ MHz) and the optical beat note
 158 were locked. Moreover, two electro-optic modulators were used in the signal oscillator to improve

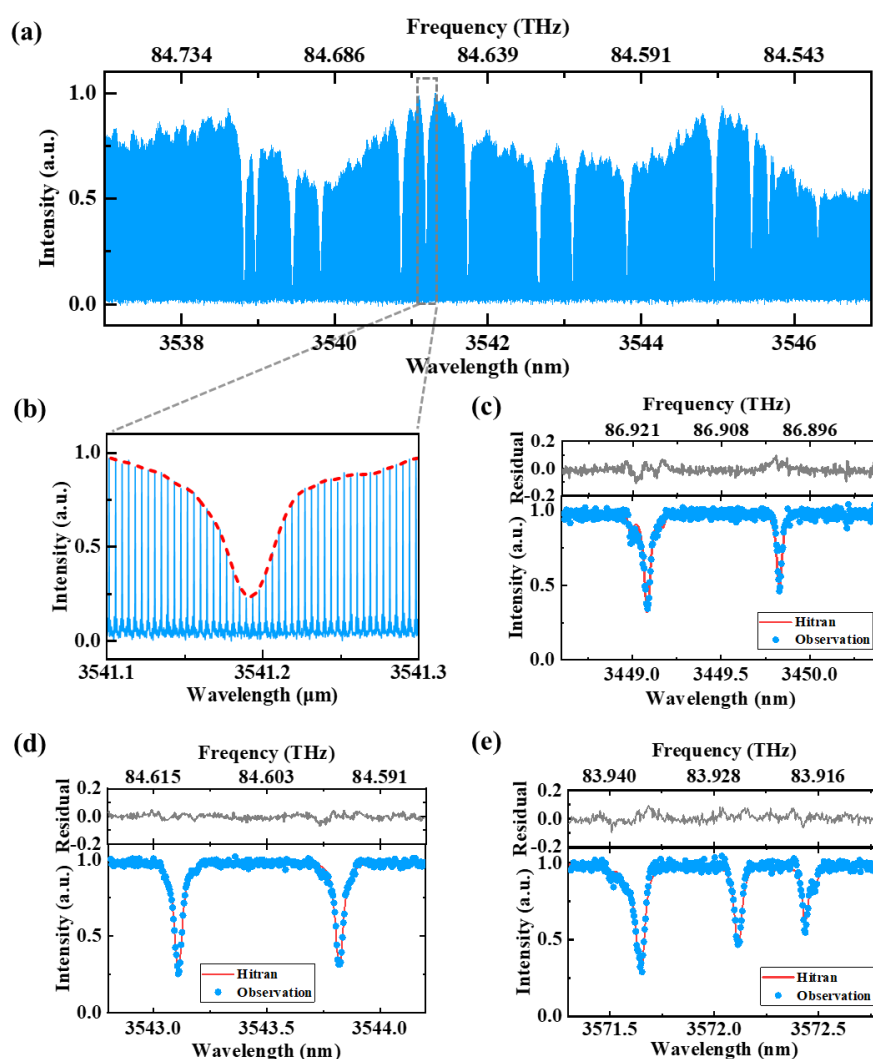
159 the modulation bandwidth of the frequency control [40]. Thereafter, two combs were delivered
 160 into two parallel IPDFG modules to generate the MIR dual-comb system. The two MIR combs
 161 could provide a broad spectrum from 2.4 to 4.2 μm . To evaluate the applicability for spectroscopy,
 162 the two MIR beams were combined to pass through an 8 cm gas cell filled with pure methane at a
 163 pressure of 150 mbar. The interferogram signal was acquired through a balanced photodetector
 164 (Qube-DT, ppqSense) equipped with two HgCdTe photodetectors (PVI-2TE-5, VIGO System).
 165 The response spectral range of the detector is 3–5 μm . In addition, two half-wavelength plates
 166 were used to control the polarization of the MIR light and optimize the signal-to-noise ratio (SNR)
 167 of the interferograms. Before the detection, we attenuated the power of the signal comb to ensure
 168 that the two beams with the same power were injected into the detector. After passing through a
 169 48 MHz electronic low-pass filter, the DCS signal was recorded using a data acquisition card with
 170 a sampling rate of 100 MHz. Figure 4(b) shows the measured interferogram signal for 150 ms. It
 171 is evident that the period of the interferograms was ~ 0.024 s, corresponding to the repetition rate
 172 difference of ~ 42 Hz. Figure 4(c) exhibits a 0.02 ms temporal domain of interferograms in which
 173 we can acquire the information in the frequency domain via further Fourier transform.



174
 175 Fig. 5. Mode-resolved MIR dual-comb spectra at different wavelength scales of (a) 1.4, (b)
 176 0.002, and (c) 0.0002 μm .

177 To retrieve the frequency-domain optical spectrum, 20 interferograms (0.5-s temporal signal)
 178 were extracted as a unit for the Fourier transform. A total of 100 s of data were recorded and
 179 coherently averaged to obtain a high SNR DCS. As illustrated in Fig. 5(a), we obtained the DCS
 180 in the range of 3.0–4.2 μm , corresponding to a frequency bandwidth of 25 THz. The retrieved dual-
 181 comb spectrum was narrower than the spectrum measured using a Fourier transform spectrometer

182 because we could not retrieve the spectrum in the 2–3 μm range owing to the limited response
 183 bandwidth (3–5 μm) of the detector. In the frequency domain, approximately 2.5×10^5 modes were
 184 resolved with a 100 MHz spectral resolution. We also calculated the figure of merit, defined as
 185 $\text{SNR} \times M / T^{1/2}$, where M is the number of comb teeth and T is the measurement time. The figure
 186 of merit was 1.03×10^6 , which is the same order of magnitude as the results in references [30, 41].
 187 In addition, the SNR of the peak spectrum, which represents the ratio of the signal to random
 188 variations of the baseline [21], was 28. Figures 5(b) and 5(c) show the mode-resolved MIR dual-
 189 comb spectra over wavelength spans of 0.002 and 0.0002 μm , respectively, confirming that the
 190 simple DCS system has the capacity for high-resolution gas sensing in the MIR region.



191

192 Fig. 6. (a) Absorption lines of methane at 3537–3547 nm region. (b) Zoom-in absorption line

193 of methane at 3541.1–3541.3 nm. (c)–(e) Comparison results of the extracted gas absorption

194 lines (blue dot) and the theoretical profiles from the HITRAN database (red line).

195 To assess the applicability of the MIR dual-comb system to high-resolution spectroscopy, we
196 measured its methane absorption spectrum. Several absorption lines in the 3537–3547 nm region
197 is shown in Fig. 6(a). A single absorption peak zoom-in in the 3541.1–3541.3 nm consists of ~50
198 comb modes with a frequency interval of ~100 MHz, as shown in Fig. 6(b). Figures 6(c)–(e) show
199 several absorption peaks (blue dots), in which all the absorption lines are consistent with the
200 standard profiles (red curves, Voigt profiles, HITRAN 2020 [42]). The RMS of the residuals in
201 Fig. 6(c)–(e) were 3.2%, 1.9% and 2.9%.

202 In the low SNR range, it is difficult to retrieve the absorption lines. Although the SNR of our
203 system can be further improved by increasing the power. The saturation power (~2 mW) of the
204 detector limited the SNR because each comb line has only nW level power. It remains a challenge
205 for dual-comb systems to achieve high SNR DCS in broadband parallel measurement. Recent work
206 has demonstrated a method of signal processing to resolve this issue in the NIR region, and the
207 ideas could be used to improve the SNR of MIR DCS [43]. In this system, the spectrum has a fast
208 baseline with tens of gigahertz linewidth, which is similar linewidth with the gas absorption line
209 at standard or high atmospheric pressure. So, we measure the gas absorption peak at low pressure
210 (150 mbar) to reduce the impact of the baseline. For broader absorption lines at standard
211 atmospheric pressure, four-point normalization correction method can be used to effectively
212 remove the effects of the baseline [1, 41, 44].

213 III. Conclusion

214 We demonstrated a simple and compact MIR dual-comb spectrometer. Using the IPDFG method,
215 we yielded broad MIR combs on chirped PPLN waveguides and developed a mode-resolved dual-
216 comb spectrometer. The spectrometer provided 100 MHz resolution in the range of 3.0–4.2 μm
217 corresponding to 25 THz bandwidth. In comparison with bulky two-branch DFG combs, the
218 proposed MIR comb system is not only more integrated but also more stable, without noise from
219 the pump-signal delay jitter. The high-efficiency PPLN waveguide reduced the power threshold
220 required to drive the IPDFG process. In addition, the lens group for waveguide coupling could be
221 replaced by an all-fiber structure. Optimization of the period distribution and channel length of the
222 waveguide would improve the MIR spectral bandwidth. This MIR dual-comb system is expected
223 to develop into more integrated measurement devices with on-chip femtosecond pulse generation,
224 amplifiers, and nonlinear broadening technologies for portable gas-sensing equipment with high
225 sensitivity and high resolution.
226

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