

# Solidification of leads: approximate solutions of non-linear problem

D.V. ALEXANDROV, A.P. MALYGIN, I.V. ALEXANDROVA

Department of Mathematical Physics, Urals State University, 51 Lenin Avenue, 620083 Ekaterinburg, Russia  
E-mail: dmitri.alexandrov@usu.ru

**ABSTRACT.** We present new analytical results relating to the growth and evolution of sea ice. It is noteworthy that thin sea ice plays a central role in the surface heat and mass balance of the Arctic Ocean. In order to describe these balances, we analyze highly resolved temperature data taken through the air/sea/ice interface during the transition from an ice-free to an ice-covered Arctic Ocean surface. Our detailed analysis of the field data is based on the classical model of a mushy layer, which is modified in order to obtain analytical solutions in explicit form (so, for example, ice thickness and growth rate, temperature distributions, conductive and latent heat fluxes are determined). Furthermore, we find that the sea-ice growth is not simply a square-root function of time. It depends on the temperature variations in the atmosphere and lies between two square-root functions of time for the maximum and minimum temperatures found during observations. The theory under consideration is in good agreement with observations.

## INTRODUCTION

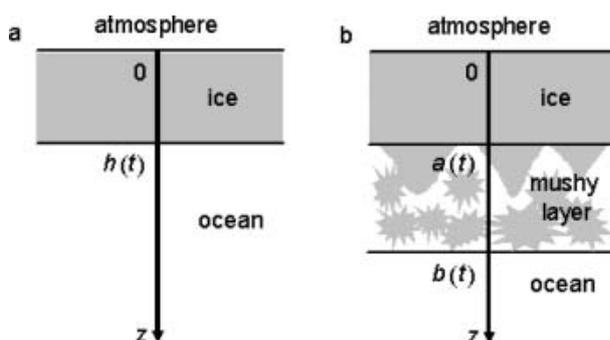
Young sea ice plays a very important role in the surface heat and mass balance of the Arctic Ocean. This ice is formed, for example, due to the divergence of wind stress which continually produces cracks in the perennial sea-ice cover, known as leads. These transient fissures attract scientific attention because they provide a thermal conduit through which heat- and radiative-transfer processes are enhanced tremendously, relative to the thick pack ice that surrounds them. The thermal importance of leads was put in context by Badgley (1966), who showed that during winter the atmospheric heat flux from rapidly freezing leads can be several orders of magnitude larger than over perennial sea ice. He emphasized the large-scale implications of leads by arguing that they need occupy only 1% of the area of the ice cover in order to dominate the heat exchange from the ocean to the atmosphere. In the Arctic winter, the relatively warm water in leads is exposed to the cold air above it. A thin veneer of ice rapidly forms across an exposed lead. After 1 day's growth, the ice layer is about 10 cm deep, which is still thin compared with the surrounding ice, which is typically several metres thick. The field observations (The LeadEx Group, 1993) show that the heat loss through leads can be up to  $300 \text{ W m}^{-2}$ , or 15 times that from the surrounding ice. We consider the initial formation

of ice in leads and its growth during the first few days. Contrary to the theory developed by Wettlaufer and others (2000), which is based on the balance approaches and phenomenological considerations, and other papers on this subject, our theory uses as a source the classical mushy (skeletal)-layer theory modified by reasonable and verified physical hypotheses. The analyticity and explicit form of all dynamic dependencies, obtained from the non-linear equations of a mushy layer, is the main feature of our approach. A detailed description of the scientific program and observations has been given by The LeadEx Group (1993) and Wettlaufer and others (2000). We will not dwell on this point in detail. However, we will point out the main features of the LeadEx experiment field campaign. There were four main lead deployments during the 6 week experiment. A particularly interesting deployment is 'lead 3' which was the largest (approximately 1 km wide) lead. Deployment at lead 3 began early on the morning of 6 April 1992 and was evacuated 2 days later. We describe observations from both of the buoys that were deployed late on the afternoon of 6 April 1992 (buoy 5 was deployed  $\sim 2$  hours before buoy 6).

At first, for the goals of our theory, we briefly outline the frontal model and discuss its predictions about sea-ice dynamics.

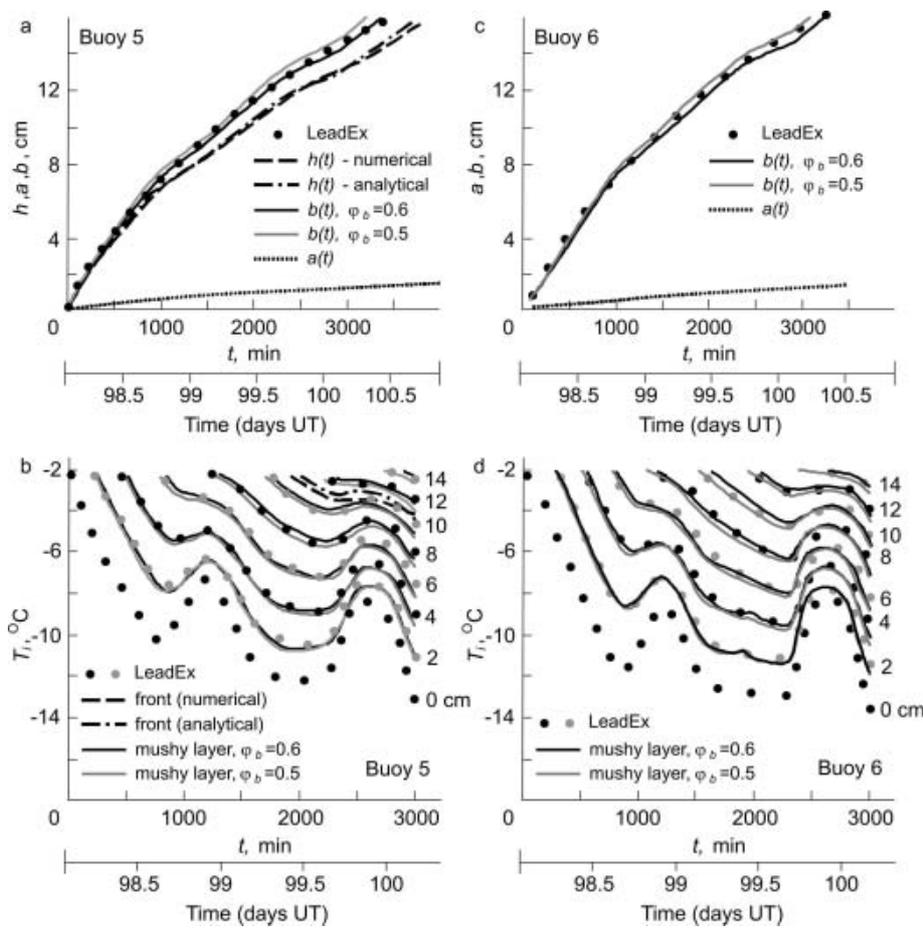
## FRONTAL APPROACH

Let us now demonstrate how one of the simplest models of the planar front works in practice. The system under consideration is shown in Figure 1a: ice and sea water are divided by the phase transition boundary,  $h(t)$ , moving downwards in the ocean because the ice surface,  $z = 0$ , is cooled with time oscillations. The atmospheric temperature,  $T_s(t)$ , determined at  $z = 0$ , will be regarded as experimentally known. Now, we treat the process as fully thermally controlled. On this basis, the heat transfer process is described by the local conservation of heat within the sea ice



**Fig. 1.** A scheme illustrating the models under consideration: (a) planar front and (b) mushy layer.

$$\frac{\partial T_i}{\partial t} = a_i \frac{\partial^2 T_i}{\partial z^2}, \quad a_i = \frac{k_i}{\rho_i c_i}, \quad 0 < z < h(t) \quad (1)$$



**Fig. 2.** Time series of ice thickness and temperature–time traces for (a, b) buoy 5 and (c, d) buoy 6 at lead 3 in accordance with the LeadEx experiment and the theory under consideration. The ice–mushy-layer boundary is a good approximation to the data for  $\varphi_b = 0.5$  and  $\varphi_b = 0.6$  (these dependencies are shown by means of function  $a(t)$ ). Numbers at the curves corresponding to each trace designate the depths (expressed in centimeters) measured from the ice/atmosphere interface. The curve at  $z = 0$  cm represents the atmospheric temperature ( $T_s(t)$ ) at the ice surface. The timescale used by the LeadEx investigators is decimal days of 1992, abbreviated as UT. The time origin in minutes corresponds to 0221, day 98 UT. Physical properties used in calculations:  $T_0 = -2^\circ\text{C}$ ,  $L_v = 3072 \times 10^5 \text{ W s m}^{-3}$ ,  $k_i = 2.03 \text{ W m}^{-1} \text{ }^\circ\text{C}^{-1}$ ,  $k_w = 0.56 \text{ W m}^{-1} \text{ }^\circ\text{C}^{-1}$ ,  $D_w = 1.2 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$ .

supplemented by the Stefan condition (a heat balance) at the planar interface, which is

$$k_i \frac{\partial T_i}{\partial z} = L_v \frac{dh}{dt}, \quad z = h(t), \quad (2)$$

where  $T_i$  is the temperature,  $L_v$  is the latent heat released as the ice fraction increases,  $k_i$  is the thermal conductivity,  $\rho_i$  is the density and  $c_i$  is the specific heat capacity of the sea ice. The ocean is treated as isothermal, which is to say that the temperature field  $T_o = \text{constant}$ , for  $z \geq h(t)$ . Analyzing experimental curves (see Fig. 2), we conclude that the temperature distribution in the young sea ice can be regarded as a nearly linear function of the spatial coordinate  $z$ . From the physical point of view, this means that the temperatures at different depths undergo near-self-similar change (Fig. 2b and d), with small variations from full self-similarity. From the mathematical point of view, this means that Equation (1) takes the form  $\partial^2 T_i(z, t) / \partial z^2 = 0$ . This is because the temperature relaxation time is many times less than a characteristic time of the front motion. Taking into account the latter, we arrive at the linear temperature profile within the sea ice

$$T_i(z, t) = T_s(t) + \frac{T_o - T_s(t)}{h(t)} z. \quad (3)$$

The position of the planar sea-ice–ocean interface is found from condition (2), namely

$$h(t) = \sqrt{\frac{2k_i}{L_v} \left( T_o t - \int_0^t T_s(\alpha) d\alpha \right)}, \quad (4)$$

where the initial condition of the form  $h(0) = 0$  is taken into account.

Time series of ice thickness and temperature–time traces in accordance with expressions (3) and (4) are shown in Figure 2a and b for buoy 5 by the dash-dotted lines. It is easily seen that this frontal solution rather poorly describes experimental data (this line is drawn only for  $z = 10$  cm in Fig. 2b). To test the validity of expressions (3) and (4) (instead of the partial differential equation (1) with corresponding boundary conditions) we demonstrate our numerical solution of expressions (1) and (2) by the dashed curves in Figure 2a and b. One can readily see that the dashed and dash-dotted curves coincide very closely, whereas, as before, the curves obtained numerically and experimentally are widely spaced.

Further, if we forget for a minute that the temperature  $T_o$  is constant, that is, if we consider it as a free time-dependent parameter, we conclude that an increase in the absolute value of  $T_o$  decreases the calculated  $h(t)$  for each fixed  $t$ , i.e.

the front positions, obtained from expression (4), moving  $h(t)$  further from experimental data. On the other hand, the temperature profiles  $T_i(z, t)$ , obtained from expression (3) for fixed  $z$ , approach experimental data for this same increase in  $|T_o|$ . Decreasing the absolute value of  $T_o$  leads to the opposite conclusions. It immediately follows that variations in the temperature  $T_o$  cannot reconcile theory and observations, or, in other words, the frontal theory does not adequately describe experimental data. This is apparently due to the fact that the clear dividing boundary 'sea-ice-ocean' of the phase transition does not exist in natural conditions. In other words, the phase transition occurs in a layer, filled with the liquid and solid material, which is ahead of the purely sea ice. Such a layer is considered below. For now, let us emphasize that the linear temperature profile (3) is in good agreement with the frontal model, and perhaps this profile describes most initial stages of the process.

### MUSHY LAYER

Mushy layers are regions of mixed phase (solid and liquid) in which the solid forms a rigid matrix and the liquid fills its interstices. We model the process under consideration by a thermodynamically equilibrium mushy layer (see, e.g., Buyevich and others, 2001). We consider a semi-infinite region ( $z > 0$ ) filled with the young sea ice ( $0 < z < a(t)$ ), the mushy layer ( $a(t) < z < b(t)$ ) and the ocean ( $z > b(t)$ ). Here  $a(t)$  and  $b(t)$  represent the sea-ice/mushy-layer and mushy-layer/ocean-phase transition boundaries (Fig. 1b). As before, our analysis is based on the assumption of a linear temperature profile in the sea ice with respect to the spatial coordinate, i.e.

$$T_i(z, t) = T_s(t) + C_1(t)z, \quad 0 < z < a(t), \quad (5)$$

where  $C_1(t)$  is a time-dependent function. This expression is based on observations by The LeadEx Group (1993) (see also Wettlaufer and others, 2000) and aforementioned discussions.

By analogy, by reason of self-similarity, the temperature profile within the mushy layer is considered as a linear function of  $z$ , i.e.

$$T_m(z, t) = T_1(t) + zT_2(t), \quad a(t) < z < b(t), \quad (6)$$

where time-dependent functions  $T_1(t)$  and  $T_2(t)$  are found below (gradients of distributions (5) and (6) are different). From the physical point of view, the temperature linearity means that the relaxation time of the temperature field is not only less than a characteristic time for growth of the mushy layer, but also less than the time of variation of solid fraction in the mushy layer. What is more, the question of why expression (6) approximately satisfies the classical heat-transfer equation

$$\rho_m c_m \frac{\partial T_m}{\partial t} = \frac{\partial}{\partial z} \left[ k_m(\varphi) \frac{\partial T_m}{\partial z} \right] + L_v \frac{\partial \varphi}{\partial t} \quad (7)$$

is discussed below. Here  $\varphi$  is the solid fraction,  $\rho_m$  is the density,  $c_m$  is the heat capacity and  $k_m$  is the conductivity of the mushy layer.

The transport of solute takes the form (we use the Scheil equation to describe the mass transfer in a mush (Kerr and others, 1990))

$$\frac{\partial}{\partial t} [(1 - \varphi)C_m] = 0, \quad a(t) < z < b(t), \quad (8)$$

where  $C_m$  is the brine salinity (integration gives the Scheil

formula known in metallurgy). Formula (8), which assumes that the salinity of the mushy layer is independent of time, has been frequently applied by a number of investigators (see, e.g., Scheil, 1942; Kerr and others, 1990). It is a good approximation for the impurity redistribution during the crystal growth for a wide range of experimental conditions (e.g. Flemings, 1974). Within the mushy layer the local salinity of the liquid phase and the local temperature are related to one another through the phase diagram for sea ice (e.g. Weeks, 1994). For the range of salinities used here, the salinity-dependent freezing point is expressed by the linear phase diagram

$$T_m = -mC_m, \quad a(t) < z < b(t), \quad (9)$$

where  $m$  is the liquidus slope.

The boundary conditions applied at the sea-ice/mushy-layer interface are (Worster, 1986)

$$\varphi = \varphi_a, \quad T_i = T_m, \quad z = a(t), \quad (10)$$

$$L_v(1 - \varphi_a) \frac{da}{dt} = k_i \frac{\partial T_i}{\partial z} - [k_i \varphi_a + k_w(1 - \varphi_a)] \frac{\partial T_m}{\partial z}, \quad z = a(t), \quad (11)$$

$$C_m(1 - \varphi_a) \frac{da}{dt} = -D_w(1 - \varphi_a) \frac{\partial C_m}{\partial z}, \quad z = a(t), \quad (12)$$

where  $\varphi_a = \varphi_a(t)$  is the solid fraction at  $z = a(t)$ , and  $k_w$  and  $D_w$  are the thermal conductivity and diffusion coefficient, respectively, of the pure water. The thermal properties of the mush are assumed to be volume-fraction-weighted averages of the properties of the individual phases, so that  $k_m(\varphi) = k_i \varphi + k_w(1 - \varphi)$  (see, e.g., Buyevich and Alexandrov, 2005).

Further, we have the boundary conditions imposed at the interface between the mushy layer and the relatively warm isothermal ocean ( $T_o = \text{const.}$ )

$$\varphi = \varphi_b, \quad T_m = T_o, \quad z = b(t), \quad (13)$$

$$L_v \varphi_b \frac{db}{dt} = [k_i \varphi_b + k_w(1 - \varphi_b)] \frac{\partial T_m}{\partial z}, \quad z = b(t), \quad (14)$$

where  $\varphi_b$  is the solid fraction at  $z = b(t)$ , and  $T_o$  is the constant temperature of the sea water determined for  $z \geq b(t)$ . It must be emphasized that the mass-balance condition at  $z = b(t)$ , analogous to the boundary condition (12), is absent within the framework of our model. This is because some variations in the temperature gradient at  $z = b(t)$  on the mush side of the interface (constant temperature in the ocean) lead to corresponding variations in the brine salinity gradient at  $z = b(t)$  and, therefore, to variations in the mushy-layer thickness in accordance with the criterion for constitutional supercooling (this condition holds for the mushy layer and its boundaries), which is

$$\frac{\partial T_m}{\partial z} = -m \frac{\partial C_m}{\partial z}.$$

Physically, a decrease in the temperature within the oceanic boundary layer causes a crystallization process, which is in progress until the local salinity attains its equilibrium value for a given temperature.

Integrating Equation (8) and taking into account expressions (6), (9) and (13), we come to the solid-phase distribution within the mushy layer (a similar form of  $\varphi$  is

deduced by Wettlaufer and others, 2000):

$$\varphi(z, t) = 1 + \frac{T_o(\varphi_b - 1)}{T_1(t) + zT_2(t)}. \tag{15}$$

Substitution of expressions (5), (6), (9) and (15) into the boundary conditions (10–14) gives

$$\varphi_a(t) = 1 + \frac{T_o(\varphi_b - 1)}{T_s(t) + C_1(t)a(t)}, \tag{16}$$

$$C_1(t) = \frac{L_V(1 - \varphi_a)}{k_i} \frac{da}{dt} + [\varphi_a + K(1 - \varphi_a)]T_2(t), \quad K = \frac{k_w}{k_i}, \tag{17}$$

$$T_s(t) + C_1(t)a(t) = T_o + T_2(t)(a(t) - b(t)), \tag{18}$$

$$[T_2(t)(b(t) - a(t)) - T_o](1 - \varphi_a) \frac{da}{dt} = D_w(1 - \varphi_a)T_2(t) \tag{19}$$

$$T_2(t) = \frac{L_V\varphi_b}{\Phi} \frac{db}{dt}, \quad \Phi = \Phi(\varphi_b) = k_i\varphi_b + k_w(1 - \varphi_b), \tag{20}$$

$$T_1(t) = T_o - b(t)T_2(t). \tag{21}$$

As is seen from expression (16), if we suppose  $\varphi_a = 1$ , it immediately follows that  $\varphi_b = 1$ , that is, the mushy layer is entirely filled with the sea ice (frontal model). In view of the fact that we seek an alternative solution ( $\varphi_a \neq 1$ ), like factors,  $1 - \varphi_a$ , can be cancelled from both sides of Equation (19).

Combining expressions (16), (18) and (20), we find the solid fraction at the ice/mushy-layer interface in the form

$$\varphi_a(t) = 1 + \frac{T_o(\varphi_b - 1)}{T_o + \frac{L_V\varphi_b}{\Phi} \frac{db}{dt} (a(t) - b(t))}. \tag{22}$$

Eliminating  $T_2(t)$  from expressions (19) and (20), we have

$$\left[ (a(t) - b(t)) \frac{L_V\varphi_b}{\Phi} \frac{db}{dt} + T_o \right] \frac{da}{dt} = - \frac{D_w L_V \varphi_b}{\Phi} \frac{db}{dt}. \tag{23}$$

In view of the fact that the interfaces move relatively slowly (The LeadEx Group, 1993; Wettlaufer and others, 2000), we arrive at the linear differential equation connecting  $a(t)$  and  $b(t)$  (neglecting the term proportional to  $(da/dt)(db/dt)$ ). Integrating this equation in view of the initial conditions  $a(0) = b(0) = 0$ , we get

$$a(t) = - \frac{D_w L_V \varphi_b}{T_o \Phi} b(t) \tag{24}$$

$(a(t)/b(t) = 0.071$  for the physical parameters under consideration and  $\varphi_b = 0.5$ ). We choose these initial conditions because a characteristic time of observations (The LeadEx Group, 1993) is many times higher than a time of mushy-layer initiation.

Substituting  $C_1(t)$  and  $T_2(t)$  from expressions (17) and (20) into condition (18), eliminating  $\varphi_a(t)$  by means of formula (22), we obtain the non-linear differential equation containing functions  $a(t)$  and  $b(t)$ :

$$\begin{aligned} & L_V T_o (\varphi_b - 1) \left[ (1 - K) \frac{\varphi_b}{\Phi} \frac{db}{dt} - \frac{1}{k_i} \frac{da}{dt} \right] a(t) \\ & = \left( T_o - T_s(t) - \frac{L_V \varphi_b}{\Phi} b(t) \frac{db}{dt} \right) \left[ (a(t) - b(t)) \frac{L_V \varphi_b}{\Phi} \frac{db}{dt} + T_o \right]. \end{aligned} \tag{25}$$

Further, substituting the term in square brackets from Equation (23) into Equation (25), taking into account

Equation (24), we come to the linear differential equation for  $b^2(t)$ :

$$\frac{1}{2} \frac{db^2}{dt} = T_o - T_s(t),$$

where

$$I = \frac{L_V \varphi_b}{\Phi} \left[ 1 - \frac{D_w L_V \varphi_b}{T_o \Phi} \left( \frac{L_V D_w}{k_i T_o} + 1 - K \right) (\varphi_b - 1) \right].$$

After integration of this equation ( $b(0) = 0$ ), we find the mushy-layer/ocean interface

$$b(t) = \sqrt{\frac{2}{I} \left( T_o t - \int_0^t T_s(\alpha) d\alpha \right)}. \tag{26}$$

Expression (26) shows that the interfaces  $a(t)$  and  $b(t)$ , as would be expected, become self-similar (Worster, 1986) if the ice surface temperature  $T_s$  is constant. If the temperature  $T_s$  undergoes different time variations, the interfaces  $a(t)$  and  $b(t)$  lie between two self-similar regimes, which correspond to the maximum ( $T_{max}$ ) and minimum ( $T_{min}$ ) ice surface temperatures measured in experiments. So, for example, for the mushy-layer/ocean interface, we have

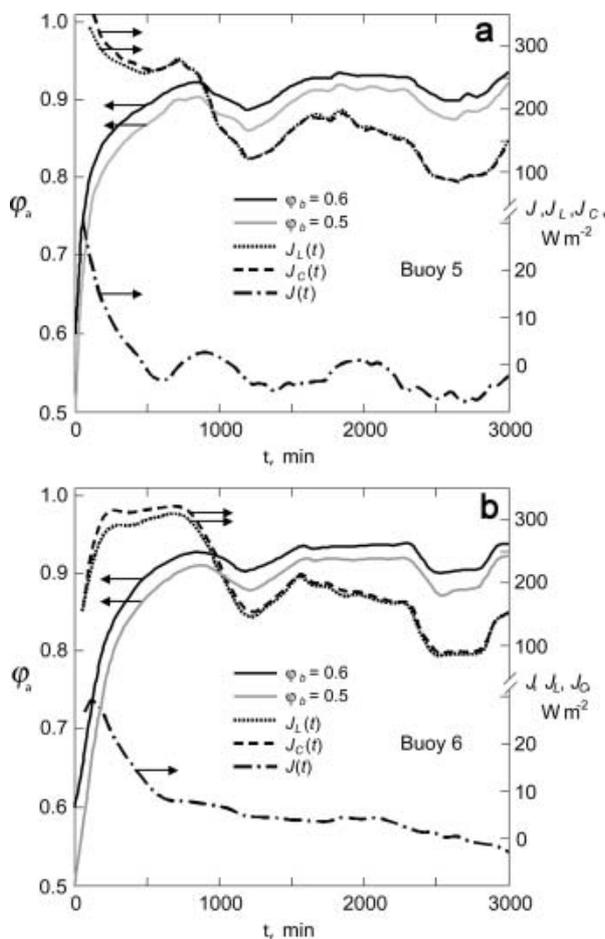
$$\sqrt{\frac{2}{I} (T_o - T_{max})} t \leq b(t) \leq \sqrt{\frac{2}{I} (T_o - T_{min})}.$$

Thus, the non-linear problem under consideration is solved analytically (explicit form of solutions is given by expressions (5), (6), (9), (15), (17), (20–22), (24) and (26)). Let us especially emphasize that the solution depends on one free parameter  $\varphi_b$  (this value cannot be found in the context of the theory under consideration). The solid fraction  $\varphi_b$  must be found semi-empirically (when one of the functions found theoretically is compared with experiments). Then all of the other functions will be completely known for any depths and times.

We have been interested to compare the mushy-layer theory with the frontal analogue. If we formally put  $\varphi_b = 1$  (the mushy layer is entirely filled with the sea ice), it is easy to see that expression (26) transforms to expression (4),  $\varphi_a(t)$  and  $\varphi(z, t) \rightarrow 1$ , and  $T_1(t)$  and  $C_1(t) = T_2(t)$  become  $T_s(t)$  and  $(T_o - T_s(t))/h(t)$ , respectively. In other words, our analytical solutions for the mushy layer transform to their analogues for the planar front.

Figure 2 demonstrates how the theory under consideration agrees with experimental data (see The LeadEx Group, 1993; Wettlaufer and others, 2000). The free parameter  $\varphi_b$  is chosen in such a manner that one of the functions found theoretically would approximate its experimental analogue (it is easily seen from Figure 2 that all of the other values found theoretically are in good agreement with observations for this value of  $\varphi_b$ ). All of the curves plotted for two values of  $\varphi_b$  essentially differ from the frontal solutions and properly describe the solidification dynamics of ice-thickness and temperature fluctuations.

The solid fraction at the sea-ice/mushy-layer interface as a function of time is shown in Figure 3. An important point is that  $\varphi_a$  and  $\varphi$  ( $\varphi_b \leq \varphi \leq \varphi_a$ ) undergo only insignificant time and spatial variations (a rapid growth of  $\varphi$  occurs only in the early stages of the process,  $\sim 100$  min, when a thin ice cover appears). Taking into account the latter and the fact that the temperature relaxation time is many times smaller than a characteristic time of the front motion, we conclude that Equation (7) can be approximated by means of equation  $\partial^2 T_m(z, t) / \partial z^2 = 0$ . Now, it is easily seen that the linear



**Fig. 3.** Time series of the solid fraction  $\varphi_a$  (scale of values on the left) and heat fluxes (scale of values on the right) for (a) buoy 5 and (b) buoy 6. Heat fluxes are calculated for  $\varphi_b = 0.5$  (buoy 5) and  $\varphi_b = 0.6$  (buoy 6).

temperature profile (6) exactly satisfies this equation and approximately describes the heat balance in the form of Equation (7). The mass-balance equation in the form of Equation (8) follows from expressions (6) and (9).

It is important to keep in mind that the sea-ice/ocean interface in nature does not divide pure ice and freezing ocean, and divides the mushy layer with a high content of ice ( $\varphi \sim 0.5\text{--}0.9$ ; Fig. 3) and sea water free of ice. The sea-ice/mushy-layer interface,  $a(t)$ , lags behind the mushy-layer/ocean interface,  $b(t)$ , by virtue of the fact that the process of ice formation is hampered within the mushy layer with a high content of ice (all of the impurities rejected by the ice lattice are initially retained within the interstices of a layer of sea ice).

Let us pay attention to the conductive heat flux released to the atmosphere from the sea-ice/atmosphere interface at  $z = 0$ . Within the framework of the model under consideration, this flux can be written in the form  $J_C(t) = k_i C_1(t)$ . This flux stems from the latent heat flux and other factors. Let us write down the mean latent heat flux as

$$J_L(t) = \frac{L_V}{b(t) - a(t)} \int_{a(t)}^{b(t)} \varphi(z, t) dz \left( \frac{db}{dt} - \frac{da}{dt} \right).$$

In view of insignificant rates of change of  $a(t)$  with time (Fig. 2a and c), the term connected with the motion of this

boundary is omitted. Figure 3 demonstrating time variations of the fluxes shows that  $J_C(t)$  and  $J_L(t)$  lie close to each other. The residual heat flux  $J(t) = J_C(t) - J_L(t)$  (see Fig. 3), within the framework of the model under consideration, is connected with the heat release to the atmosphere. In order to explain the latter it is necessary to say that the residual flux is significant only during initial stages of the process (Figure 3 illustrates its dynamics hereafter, where the flux drops and oscillates in the vicinity of  $J = 0$ ). In other words, the role of  $J$  makes itself evident during essential variations in the solid fraction. It should be noted that the heat flux  $J(t)$  decreases when the atmospheric temperature goes down and, as a consequence, when the mushy layer increases most rapidly (these instants of time are shown by slight crests of  $b(t)$  in Figure 2a and c). The total oceanic heat flux differs from the residual flux  $J(t)$  because some additions (e.g. the turbulent oceanic heat flux at the underside of the ice, and the solar radiation heat flux reflected from the ice cover) appear in nature. Some of these factors can be analyzed in the spirit of this paper. Let us emphasize in conclusion that the heat flux  $J_C(t)$  (or  $J_L(t)$ ), obtained theoretically on the basis of experimental data, approximately represents the total heat flux per unit area lost in solidification of leads.

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